

5 **PHOSPHOR BASED LIGHT SOURCES UTILIZING TOTAL INTERNAL
REFLECTION**

CROSS-REFERENCE

This application claims the benefit of U.S. Provisional Application Nos.
10 60/443,274, 60/443,232, and 60/443,235 all filed 27 January 2003, and all
incorporated by reference herein.

RELATED PATENT APPLICATIONS

The following co-owned and pending U.S. patent applications are
15 incorporated herein by reference: "PHOSPHOR BASED LIGHT SOURCES HAVING
A POLYMERIC LONG PASS REFLECTOR", U.S. Application Serial No.
10/726,997; "METHODS OF MAKING PHOSPHOR BASED LIGHT SOURCES
HAVING AN INTERFERENCE REFLECTOR", U.S. Application Serial No.
10/727,023; "PHOSPHOR BASED LIGHT SOURCE COMPONENT AND
20 METHOD OF MAKING", U.S. Application Serial No. 10/726,790; "PHOSPHOR
BASED LIGHT SOURCE HAVING A FLEXIBLE SHORT PASS REFLECTOR",
U.S. Application Serial No. 10/726,995; "PHOSPHOR BASED LIGHT SOURCES
HAVING A NON-PLANAR LONG PASS REFLECTOR", U.S. Application Serial
No. 10/727,072; "PHOSPHOR BASED LIGHT SOURCES HAVING A NON-
25 PLANAR LONG PASS REFLECTOR AND METHOD OF MAKING", U.S.
Application Serial No. 10/727,026; and "PHOSPHOR BASED LIGHT SOURCES
HAVING A NON-PLANAR SHORT PASS REFLECTOR AND METHOD OF
MAKING", U.S. Application Serial No. 10/726,968; all filed 02 December 2003.

In addition, the following co-owned and pending U.S. patent applications are
30 incorporated by reference: "PHOSPHOR BASED LIGHT SOURCES HAVING
FRONT ILLUMINATION", Attorney Docket No. 58388US004; and "PHOSPHOR

FIELD OF THE INVENTION

5 The present invention relates to light sources. More particularly, the present invention relates to light sources in which light emitted from a light emitting diode (LED) impinges upon and excites a phosphor material, which in turn emits visible light.

DISCUSSION

10 White light sources that utilize LEDs in their construction can have two basic configurations. In one, referred to herein as direct emissive LEDs, white light is generated by direct emission of different colored LEDs. Examples include a combination of a red LED, a green LED, and a blue LED, and a combination of a blue
15 LED and a yellow LED. In the other basic configuration, referred to herein as LED-excited phosphor-based light sources (PLEDs), a single LED generates a beam in a narrow range of wavelengths, which beam impinges upon and excites a phosphor material to produce visible light. The phosphor can comprise a mixture or combination of distinct phosphor materials, and the light emitted by the phosphor can
20 include a plurality of narrow emission lines distributed over the visible wavelength range such that the emitted light appears substantially white to the unaided human eye.

 An example of a PLED is a blue LED illuminating a phosphor that converts blue to both red and green wavelengths. A portion of the blue excitation light is not absorbed by the phosphor, and the residual blue excitation light is combined with the
25 red and green light emitted by the phosphor. Another example of a PLED is an ultraviolet (UV) LED illuminating a phosphor that absorbs and converts UV light to red, green, and blue light.

 Advantages of white light PLEDs over direct emission white LEDs include better color stability as a function of device aging and temperature, and better batch-to-

batch and device-to-device color uniformity/repeatability. However, PLEDs can be less efficient than direct emission LEDs, due in part to inefficiencies in the process of light absorption and re-emission by the phosphor.

5 A white light PLED can comprise a UV emitting semiconductor die (chip) in a reflective heat sink. The reflective heat sink can also serve to partially collimate the UV light. The UV light illuminates the underside of a phosphor-containing layer, which absorbs at least a portion of the UV light and emits light at multiple wavelengths in the visible region to provide a source appearing substantially white to the ordinary observer. FIG. 1 shows one configuration of such a PLED 10. The PLED
10 includes a semiconducting LED 12 mounted in a well of an electrically conductive heat sink 14 that also reflects some of the light emitted from LED 12 toward a phosphor-reflector assembly 16. The assembly 16 can reside in an optically transparent potting material 18 which can be shaped to provide a lens feature 20 to tailor the light emitted by PLED 10. The phosphor assembly 16 is shown in greater
15 detail in FIG. 2. The phosphor is formed into a layer 22 from a combination of one or more phosphor materials mixed with a binder. A long-pass (LP) reflector 24, that reflects the UV excitation light but transmits the visible emitted light, can be applied to the top surface of phosphor layer 22. A short-pass (SP) reflector 26, that reflects visible light but transmits UV light, can be applied to the bottom of layer 22.

20 The optimum thickness of the phosphor layer for a given phosphor concentration is a compromise between efficiently absorbing the UV light (favoring an optically thick phosphor layer) and efficiently emitting visible light (favoring an optically thin phosphor layer). Further, since the intensity of UV light is greatest at the bottom of phosphor layer 22, and useful light is being extracted from the top of
25 phosphor layer 22, increasing the thickness of phosphor layer 22 above the optimum thickness will rapidly reduce overall PLED output and efficiency.

The presence of LP reflector 24 and SP reflector 26 can enhance the efficiency of PLED 10. The LP reflector 24 reflects the UV light that is not absorbed by phosphor layer 22, and that would otherwise be wasted, back onto the phosphor layer

22. This increases the effective path length of the UV light through the phosphor layer, increasing the amount of UV light absorbed by the phosphor for a given phosphor layer thickness. The optimum phosphor layer thickness can thus be reduced compared to a construction without LP reflector 24, increasing the efficiency of light generation.

Another significant loss in the PLED is due to the directionally uncontrolled generation of light in the phosphor layer, resulting in half of the visible light generated in phosphor layer 22 being directed back towards the LED. Some of this light can be captured by reflection off the sloped walls of the heat sink, but much of the light is scattered, absorbed, or reduced in quality. This loss can be reduced by placing SP reflector 26 as shown between LED 12 and phosphor layer 22.

It would be advantageous to even further enhance the efficiency of PLED constructions. It would also be advantageous to simplify and reduce the cost of manufacture of PLEDs.

BRIEF SUMMARY

The present application discloses PLEDs that utilize polymer multilayer optical films for the filtering components, i.e., the LP and SP reflectors. The multilayer optical films include individual optical layers, at least some of which can be birefringent, arranged into optical repeat units through the thickness of the film. Adjacent optical layers have refractive index relationships that maintain reflectivity and avoid leakage of p-polarized light at moderate to high incidence angles. The SP reflector comprises optical repeat units having a thickness gradient that produces a reflection band positioned to reflect visible light emitted by the phosphor and transmit UV excitation light. The LP reflector comprises optical repeat units having a different thickness gradient that produces a reflection band positioned to reflect the UV excitation light and transmit the visible light emitted by the phosphor. As a component of the PLED, the polymer multilayer optical film(s) can have a flat

configuration or at least one can be embossed or otherwise shaped to be curved, whether in the shape of a sphere, paraboloid, ellipsoid, or other shape.

Methods of manufacturing PLEDs are disclosed, which methods include forming a sheet material that includes at least one polymer multilayer optical film and a phosphor layer. In some cases the phosphor can be sandwiched between two polymer multilayer optical films: one SP reflector, and one LP reflector. In other cases the phosphor layer can be applied to only one polymer multilayer optical film. The polymer multilayer optical film(s) and phosphor layer form a phosphor-reflector assembly. Individual pieces of the phosphor-reflector assembly can be cut from the sheet material and subsequently immersed in a transparent potting material or injection-molded to form a first optical component which is then coupled to a separately manufactured LED component. The sheet material can include a carrier film to hold and store the phosphor-reflector assembly pieces in a convenient roll form until needed. The PLED can be made by joining a lower portion comprising the LED to an upper portion comprising a phosphor-reflector assembly. Also in some cases the sheet material can be embossed

The present specification discloses PLED embodiments in which a curved LP reflector is spaced apart from the phosphor layer, or at least from a central bright portion thereof, so that any UV excitation light not absorbed by the phosphor layer will impinge on the LP reflector over a limited range of incidence angles and be more efficiently reflected back onto the phosphor layer.

The present application discloses PLED embodiments that utilize an air gap proximate at least one of the multilayer optical films and the phosphor layer to promote total internal reflection.

The present application discloses PLED embodiments that utilize combinations of non-imaging concentrator elements to enhance the performance of the LP and/or SP reflector.

The present application also discloses PLED embodiments in which the LED, the LP reflector, and the phosphor layer are arranged such that excitation light from the LED is reflected directly onto a front major surface of the phosphor layer.

5 These and other aspects of disclosed embodiments will be apparent from the detailed description below. In no event, however, should the above summaries be construed as limitations on claimed subject matter, which subject matter is defined solely by the attached claims, as may be amended during prosecution.

BRIEF DESCRIPTION OF THE DRAWINGS

10 Throughout the specification, reference is made to the appended drawings, where like reference numerals designate like elements, and wherein:

FIG. 1 is a schematic sectional view of a LED-excited phosphor-based light source (PLED);

15 FIG. 2 is a sectional view of a phosphor-reflector assembly used in the source of FIG. 1;

FIG. 3 depicts a roll comprising a phosphor-reflector assembly in sheet form and subdivided into individual pieces;

FIG. 4 is a schematic sectional view illustrating individual pieces of the phosphor-reflector assembly on a carrier film;

20 FIGS. 5-7 are schematic sectional views of alternative PLED constructions;

FIG. 8 depicts a portion of still another PLED construction;

FIG. 9 is a schematic sectional view of still another PLED construction;

FIG. 10 is a schematic side view of another PLED construction that utilizes front surface illumination, as does the embodiment of FIG. 9;

25 FIG. 11 is a schematic side view of a PLED construction that makes use of an arrangement of nonimaging concentrators;

FIG. 12 is a close-up view of a portion of FIG. 11;

FIGS. 13-15 are schematic sectional views of other embodiments of a PLED construction;

FIG. 16 depicts a portion of still another PLED construction;

FIG. 17 is a graph of a light intensity spectrum of Examples 1 and 2;

FIG. 18 is a graph of a light intensity spectrum of Examples 3, 4, and 5;

FIG. 19 is a graph of a light intensity spectrum of Examples 6, 7, and 8; and

5 FIG. 20 is a graph of a light intensity spectrum of Examples 9 and 10.

DETAILED DESCRIPTION OF ILLUSTRATIVE EMBODIMENTS

While the use of one or both of LP reflector 24 and SP reflector 26 as shown in
10 FIGS. 1-2 can improve system efficiency, the improvement is limited due to certain
reflectors' poor spectral selectivity and poor reflectivity at oblique angles of incidence.
LP mirrors or filters based on scattering processes can achieve relatively constant
performance as a function of incidence angle, but have poor spectral selectivity. LP
and SP mirrors constructed from an inorganic dielectric material stack can have good
15 spectral selectivity over a narrow range of incidence angles, but suffer from spectral
blue-shifts with increasing incidence angle and low reflectivity (high transmission) of
p-polarized light at moderate to high incidence angles. Since phosphor particles
scatter the UV excitation light, and emit their own light over a wide range of angles,
conventional LP and SP mirrors are not highly effective in managing light within the
20 phosphor-reflector assembly.

The performance of PLEDs can be increased by using polymeric multilayer
optical films, i.e., films having tens, hundreds, or thousands of alternating layers of at
least a first and second polymer material, whose thicknesses and refractive indices are
selected to achieve a desired reflectivity in a desired portion of the spectrum, such as a
25 reflection band limited to UV wavelengths or a reflection band limited to visible
wavelengths. See, for example, U.S. Patent 5,882,774 (Jonza et al.). Although
reflection bands produced by these films also experience a blue-shift with incidence
angle similar to the blue-shift associated with stacks of inorganic isotropic materials,
the polymeric multilayer optical films can be processed so that adjacent layer pairs

have matching or near-matching, or deliberately mismatched refractive indices associated with a z-axis normal to the film such that the reflectivity of each interface between adjacent layers, for p-polarized light, decreases slowly with angle of incidence, is substantially independent of angle of incidence, or increases with angle of incidence away from the normal. Hence, such polymeric multilayer optical films can maintain high reflectivity levels for p-polarized light even at highly oblique incidence angles, reducing the amount of p-polarized light transmitted by the reflective films compared to conventional inorganic isotropic stack reflectors. In order to achieve these properties, the polymer materials and processing conditions are selected so that, for each pair of adjacent optical layers, the difference in refractive index along the z-axis (parallel to the thickness of the film) is no more than a fraction of the refractive index difference along the x- or y- (in-plane) axes, the fraction being 0.5, 0.25, or even 0.1. Alternatively, the refractive index difference along the z-axis can be opposite in sign to the in-plane refractive index differences.

The use of polymeric multilayer optical films also makes available a variety of new PLED embodiments and methods of construction due to the flexibility and formability of such films, whether or not they also have the refractive index relationships referred to above. For example, polymeric multilayer optical film can be permanently deformed by embossing, thermoforming, or other known means to have a 3-dimensional shape such as a portion of a paraboloid, a sphere, or an ellipsoid. See generally published application US 2002/0154406 (Merrill et al.). See also U.S. Patent 5,540,978 (Schrenk) for additional polymeric multilayer film embodiments. Unlike conventional inorganic isotropic stacks, which are normally vapor deposited layer-by-layer onto a rigid, brittle substrate, polymeric multilayer optical films can be made in high volume roll form, and can also be laminated to other films and coated, and can be die cut or otherwise subdivided into small pieces for easy incorporation into an optical system such as a PLED as further explained below. Suitable methods of subdividing polymeric multilayer optical film are disclosed in pending U.S. Application Serial No. 10/268,118, filed October 10, 2002.

A wide variety of polymer materials are suitable for use in multilayer optical films for PLEDs. However, particularly where the PLED comprises a white-light phosphor emitter coupled with a UV LED excitation source, the multilayer optical film preferably comprises alternating polymer layers composed of materials that resist degradation when exposed to UV light. In this regard, a particularly preferred polymer pair is polyethylene terephthalate (PET)/co-polymethylmethacrylate (co-PMMA). The UV stability of polymeric reflectors can also be increased by the incorporation of non-UV absorbing light stabilizers such as hindered amine light stabilizers (HALS). In some cases the polymeric multilayer optical film can also include transparent metal or metal oxide layers. See e.g. PCT Publication WO 97/01778 (Ouderkirk et al.). In applications that use particularly high intensity UV light that would unacceptably degrade even robust polymer material combinations, it may be beneficial to use inorganic materials to form the multilayer stack. The inorganic material layers can be isotropic, or can be made to exhibit form birefringence as described in PCT Publication WO 01/75490 (Weber) and thus have the beneficial refractive index relationships that yield enhanced p-polarization reflectivity as described above. However, in most cases it is most convenient and cost effective for the multilayer optical film to be substantially completely polymeric, free of inorganic materials.

FIG. 3 depicts a roll of sheet material 30, which material comprises at least one polymeric multilayer optical film and a substantially uniform phosphor layer applied to the multilayer optical film by a coating operation. The sheet material can also comprise a second polymeric multilayer optical film applied in such a way that the phosphor layer is sandwiched between the first and second polymeric multilayer optical film, as seen in FIG. 2. Additional layers and coatings providing desired mechanical, chemical, and/or optical properties can also be included. See U.S. Patent 6,368,699 (Gilbert et al.). The sheet material 30 also preferably includes a carrier film. The sheet material is kiss-cut by mechanical means such as a knife, precision die cutting, or by scanning laser radiation as described in the pending '118 application referred to above. The kiss-cut lines define discrete pieces 32 of the sheet material,

but exclusive of the carrier film which remains intact. The pieces 32 can have a cross-sectional construction similar to that shown in FIG. 2, and can be of arbitrarily small size. They are conveniently carried by the underlying carrier film 34 as shown in FIG. 4. During production of the PLEDs—and independent of the construction of the LED source—pieces 32 can be removed from the carrier film and placed in individual molds to which potting material is, or was previously, added, thus forming PLEDs as depicted in FIG. 1 but wherein the reflector components use polymeric multilayer optical films.

FIGS. 5-7 depict alternative constructions of PLEDs utilizing a concave-shaped multilayer optical film LP reflector. Spacing the LP reflector away from the phosphor and curving it in towards the phosphor and towards the LED 12 helps reduce the range of incidence angles of excitation light impinging on the LP reflector, thereby reducing the leakage of UV light through the LP reflector caused by the blue-shift effect discussed above. Preferably the multilayer optical film is permanently deformed by embossing or other suitable process into a concave surface of suitable shape before immersion in transparent medium 18. The multilayer optical films, whether LP or SP, are specular reflectors within their respective reflection bands. Diffuse reflection from a multilayer optical film is typically negligible.

In FIG. 5, PLED 40 includes a relatively small area phosphor layer 42 disposed on an optional SP reflector 44 composed of a polymeric multilayer optical film. LP reflector 46 has been embossed to acquire a concave shape and positioned next to the other components (42, 44) of the phosphor-reflector assembly. LED 12 and heat sink 14 are arranged to direct UV excitation light emitted by the LED toward the central portion of phosphor layer 42. Preferably, the UV light has its highest fluence at or near the center of phosphor layer 42. UV light not absorbed in its initial traversal of phosphor layer 42 passes through a region 48 between LP reflector 46 and phosphor layer 42 before being reflected by LP reflector 46 back towards the phosphor layer. The region 48 can be composed of transparent potting material 18, or alternatively of

another polymeric material, or air (or other gas), or glass. LP reflector 46 is preferably shaped to maximize the amount of UV excitation light reflected back to the phosphor.

FIG. 6 shows a PLED 50 similar to PLED 40, except that the size of the phosphor layer 52, SP reflector 54, and LP reflector 56 are increased. For a given distance from LED 12 to the phosphor layer, and the same heat sink 14 geometry, the larger LP reflector 56 will yield a higher concentration of light in the center of the phosphor layer. The smaller, central emitting area of the phosphor layer presents a smaller range of incidence angles of phosphor-emitted light to the surface of the LP reflector, improving overall PLED efficiency. As before, region 58 can be composed of potting material 18 or another polymeric material, or air (or other gas), or glass.

PLED 60, shown in FIG. 7, is similar to PLED 50, except the LP reflector 66 now forms an outer surface of the light source. Region 68 can be filled with potting material 18 or other transparent medium.

The phosphor layers of FIGS. 5-7 can be continuous, or patterned to limit the phosphor to where it is most effective. Moreover, in the embodiments of FIGS. 1 and 5-7 and other embodiments where the phosphor-reflector assembly is disposed above and spaced apart from the LED, the PLED can be manufactured in two halves: one containing the LED with heat sink, and the other containing the phosphor layer and multilayer reflector(s). The two halves can be made separately, and then be joined or otherwise secured together. This construction technique can help simplify manufacturing and increase overall yields.

FIG. 8 demonstrates a concept that can be applied beneficially to the other embodiments herein: providing an air gap between the LED and the phosphor layer, and/or providing an air gap proximate to one or more elements of the phosphor-reflector assembly. Only some elements of a PLED are shown in the figure for simplicity of description. An air gap 70 is shown between LED 12 and phosphor layer 72, adjacent multilayer optical film SP reflector 74. The air gap has a minimal detrimental effect on UV light from the LED reaching the phosphor layer because of the relatively small angles involved. But the air gap enables total internal reflection

(TIR) of light traveling at high incidence angles, such as light traveling in the SP reflector, the phosphor layer, and the LP reflector. In the embodiment of FIG. 8 the efficiency of the SP reflector is enhanced by allowing TIR at the lower surface of reflector 74. Alternatively, SP reflector 74 can be eliminated and the air gap can be formed directly under phosphor layer 72. An air gap can also be formed at the upper side of phosphor layer 72, or adjacent to the LP reflector at its upper or lower surface. One approach for providing the air gap involves the use of known microstructured films. Such films have a substantially flat surface opposed to a microstructured surface. The microstructured surface can be characterized by a single set of linear v-shaped grooves or prisms, multiple intersecting sets of v-shaped grooves that define arrays of tiny pyramids, one or more sets of narrow ridges, and so forth. When the microstructured surface of such a film is placed against another flat film, air gaps are formed between the uppermost portions of the microstructured surface.

As phosphors convert light of one wavelength (the excitation wavelength) to other wavelengths (the emitted wavelengths), heat is produced. The presence of an air gap near the phosphor may significantly reduce heat transmission from the phosphor to surrounding materials. The reduced heat transfer can be compensated for in other ways, such as by providing a layer of glass or transparent ceramic near the phosphor layer that can remove heat laterally.

Still another approach of improving the efficiency of PLEDs is to configure the LED, phosphor layer, and LP reflector such that at least some of the UV light from the LED is reflected by the LP reflector directly onto the top (viewing) surface of the phosphor layer, rather than directing all of the UV light onto the bottom surface of the phosphor layer. FIG. 9 shows such a PLED 80. The heat sink 14' has been modified from above embodiments so that the LED 12 and the phosphor layer 82 can be mounted generally co-planar. An SP reflector is shown underneath the phosphor layer, but in many cases will not be required. This is because LP reflector 86, which has been embossed in the form of a concave ellipsoid or similar shape, directs UV excitation light directly from the LED onto the upper surface of phosphor layer 82,

which surface faces the front of PLED 80. The LED and phosphor layer are preferably disposed at the foci of the ellipsoid. The visible light emitted by the phosphor layer is transmitted by LP reflector 86 and collected by the rounded front end of the PLED body to form the desired pattern or visible (preferably white) light.

5 Directing excitation light directly at the front surface of the phosphor layer has a number of benefits. The brightest portion of the phosphor layer—where the excitation light is the strongest—now is exposed at the front of the device rather than being obscured through the thickness of the phosphor layer. The phosphor layer can be made substantially thicker so that it absorbs substantially all of the UV excitation
10 light, without concern for the thickness/brightness tradeoff referred to above. The phosphor can be mounted on a broadband metal mirror, including silver or enhanced aluminum.

FIG. 10 shows schematically another PLED embodiment where the LED light impinges on the front surface of the phosphor layer, but wherein some of the LED
15 light also impinges on the back surface. In this embodiment, some light emitted by LED 12 impinges on the back surface of phosphor layer 92, but some LED light also reflects off of the concave-shaped LP reflector 96 to strike the front surface of phosphor layer 92 without traversing through the phosphor. Visible light emitted by phosphor layer 92 then passes through the LP reflector 96 towards the viewer or object
20 to be illuminated. The LED, phosphor layer, and LP reflector can all be immersed or attached to a transparent potting medium as shown in previous embodiments.

FIG. 11 shows schematically another PLED embodiment, wherein combinations of non-imaging concentrators are arranged to enhance the operation of the multilayer optical films. Specifically, concentrator elements 100a, 100b, 100c are
25 provided as shown between the LED 12, SP reflector 104, phosphor layer 102, and LP reflector 106. The concentrator elements have the effect of reducing the angular spread of light impinging on the multilayer reflectors, thus reducing the blue-shift of the reflection band discussed above in connection with FIGS. 5-7. The concentrator elements may be in the form of simple conical sections with flat sidewalls, or the

sidewalls can take on a more complex curved shape as is known to enhance collimation or focusing action depending on the direction of travel of the light. In any event the sidewalls of the concentrator elements are reflective and the two ends (one small, one large) are not. In FIG. 11, LED 12 is disposed at the small end of

5 concentrator 100a. Concentrator element 100a collects a wide angular range of light emitted by the LED, which range is reduced by the time such light has traveled to the large end of concentrator element 100a, where SP reflector 104 is mounted. The SP reflector transmits the UV excitation light to concentrator element 100b, which concentrates such light onto phosphor layer 102 (while increasing the angular spread

10 of the light). Wide angular range visible light emitted downwardly by phosphor layer 102 is converted by concentrator element 100b to a more narrow angular range at SP reflector 104, where it is reflected back up towards the phosphor layer 102. Meanwhile, UV light that leaks through phosphor layer 102 and visible light emitted upwardly by phosphor layer 102 initially has a wide angular spread, but is converted

15 by concentrator element 100c to a smaller angular spread so that LP reflector 106 will better transmit the visible light emitted by the phosphor and reflect the UV light back towards the phosphor layer.

To capture as much LED excitation light as possible, the small end of concentrator element 100a can have a cavity so as to capture at least some light

20 emitted by the sides of the LED, as shown in FIG. 12.

The embodiments disclosed herein are operative with a variety of phosphor materials. The phosphor materials are typically inorganic in composition, having excitation wavelengths in the 300-450 nanometer range and emission wavelengths in the visible wavelength range. In the case of phosphor materials having a narrow

25 emission wavelength range, a mixture of phosphor materials can be formulated to achieve the desired color balance, as perceived by the viewer, for example a mixture of red-, green- and blue-emitting phosphors. Phosphor materials having broader emission bands are useful for phosphor mixtures having higher color rendition indices. Desirably, phosphors should have fast radiative decay rates. A phosphor blend can

comprise phosphor particles in the 1-25 micron size range dispersed in a binder such as, for example, epoxy, adhesive, silicone, fluorocarbon, or a polymeric matrix, which can then be applied to a substrate, such as an LED or a film. Phosphors that convert light in the range of about 300 to 470 nm to longer wavelengths are well known in the art. See, for example, the line of phosphors offered by Phosphor Technology Ltd., Essex, England. Phosphors include rare-earth doped garnets, silicates, and other ceramics. The term “phosphor” as used herein can also include organic fluorescent materials, including fluorescent dyes and pigments. Materials with high stability under 300-470 nm radiation are preferred, particularly inorganic phosphors.

10

Glossary of Certain Terms

LED: a diode that emits light, whether visible, ultraviolet, or infrared, and whether coherent or incoherent. The term as used herein includes incoherent (and usually inexpensive) epoxy-encased semiconductor devices marketed as “LEDs”, whether of the conventional or super-radiant variety. The term as used herein also includes semiconductor laser diodes.

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Visible Light: light that is perceptible to the unaided human eye, generally in the wavelength range from about 400 to 700 nm.

Optical Repeat Unit (“ORU”): a stack of at least two individual layers which repeats across the thickness of a multilayer optical film, though corresponding repeating layers need not have the same thickness.

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Optical thickness: the physical thickness of a given body times its refractive index. In general, this is a function of wavelength and polarization.

Reflection band: a spectral region of relatively high reflectance bounded on either side by regions of relatively low reflectance.

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Ultraviolet (UV): light whose wavelength is in the range from about 300 to about 400 nm.

White light: light that stimulates the red, green, and blue sensors in the human eye to yield an appearance that an ordinary observer would consider “white”. Such

light may be biased to the red (commonly referred to as warm white light) or to the blue (commonly referred to as cool white light). Such light can have a color rendition index of up to 100.

5 Further Discussion

The interference reflector described herein includes reflectors that are formed of organic, inorganic or a combination of organic and inorganic materials. The terms “interference reflector” and “interference filter” as used herein are interchangeable. An interference reflector includes any reflector having a plurality of thin layers or
10 other structures that produce constructive or destructive interference of light to influence the reflective properties of the reflector. The interference reflector can be a multilayer interference reflector. The interference reflector can be a flexible interference reflector. A flexible interference reflector can be formed from polymeric, non-polymeric materials, or polymeric and non-polymeric materials. Exemplary films
15 including a polymeric and non-polymeric material are disclosed in U.S. Patent Nos. 6,010,751 and 6,172,810 and EP 733,919A2, all incorporated by reference herein.

The interference reflector described herein can be formed from flexible, plastic, or deformable materials and can itself be flexible, plastic or deformable. These interference reflectors can be deflectable or curved to a radius usable with
20 conventional LEDs, i.e., from 0.5 to 5 mm. These flexible interference reflectors can be deflected or curved and still retain its pre-deflection optical properties.

Known self-assembled periodic structures, such as cholesteric reflecting polarizers and certain block copolymers, are considered to be multilayer interference reflectors for purposes of this application. Cholesteric mirrors can be made using a
25 combination of left and right handed chiral pitch elements.

In an illustrative embodiment, a long-pass reflector or filter that partially transmits all wavelengths of blue light can be used in combination with a thin yellow phosphor layer in order to direct some blue light from the LED back onto the phosphor layer after the first pass through the phosphor.

In addition to providing reflection of UV light, a function of the multilayer optical film can be to block transmission of UV light so as to prevent degradation of subsequent elements inside or outside the LED package, including prevention of human eye damage. In some embodiments, it may be advantageous to incorporate a UV absorber on the side of the UV reflector furthest away from the LED. This UV absorber can be in, on, or adjacent to the multilayer optical film.

Although a variety of methods are known in the art for producing interference filters or reflectors, an all polymer construction can offer several manufacturing and cost benefits. If high temperature polymers with high optical transmission and large index differentials are utilized in the interference filter or reflector, then an environmentally stable filter that is both thin and very flexible can be manufactured to meet the optical needs of short-pass (SP) and (LP) filters or reflectors. In particular, coextruded multilayer interference filters or reflectors as taught in US 6,531,230 (Weber et al.) can provide precise wavelength selection as well as large area, cost effective manufacturing. The use of polymer pairs having high index differentials allows the construction of very thin, highly reflective mirrors that are freestanding, i.e. have no substrate but are still easily processed. Such interference structures will not crack or shatter or otherwise degrade either when thermoformed or when flexed to a radius of curvature as small as 1 mm.

An all polymeric interference reflector or filter can be thermoformed into various 3D shapes such as e.g. hemispherical domes (as described below). However, care must be taken to control the thinning to the correct amount over the entire surface of the dome to create the desired angular performance. Filters having a simple two dimensional curvature are easier to create than 3D, compound shaped filters. In particular, any thin and flexible filter can be bent into a 2D shaped such as e.g. a part of a cylinder, in this case an all polymeric filter is not needed. Multilayer inorganic filters on thin polymeric substrates can be shaped in this manner, as well as can inorganic multilayers on glass substrates that are less than 200 microns in thickness.

The latter may have to be heated to temperatures near the glass transition point to obtain a permanent shape with low stress.

Optimum bandedges for long and short pass filters or reflectors will depend on the emission spectra of both the LED and the phosphor in the system that the filters are designed to operate in. In an illustrative embodiment, for a short pass filter or reflector, substantially all of the LED emission passes through the filter to excite the phosphor, and substantially all of the phosphor emissions are reflected by the filter so they do not enter the LED or its base structure where they could be absorbed. For this reason, the short pass defining bandedge is placed in a region between the average emission wavelength of the LED and the average emission wavelength of the phosphor. In an illustrative embodiment, the filter is placed between the LED and the phosphor. If however, the filter is planar, the emissions from a typical LED will strike the filter at a variety of angles, and at some angle of incidence be reflected by the filter and fail to reach the phosphor. Unless the filter is curved to maintain a nearly constant angle of incidence, one may desire to place the design bandedge at a wavelength larger than the midpoint of the phosphor and LED emission curves to optimize the overall system performance. In particular, very little of the phosphor emission is directed to the filter near zero degrees angle of incidence because the included solid angle is very small.

In another illustrative embodiment, long pass reflective filters are placed opposite the phosphor layer from the LED in order to recycle the LED excitation light back to the phosphor in order to improve system efficiency. In the illustrative embodiment, a long pass reflector or filter may be omitted if the LED emissions are in the visible spectrum and large amounts are needed to balance the phosphor color output. However, a long pass filter that partially transmits the shortwave light, such as e.g. blue light, can be used to optimize the angular performance of a blue-LED/yellow-phosphor system via the spectral angle shift that would pass more blue light at higher angles than at normal incidence.

In a further illustrative embodiment, the LP filter is curved, in order to maintain a nearly constant angle of incidence of the LED emitted light on the filter. In this embodiment, the phosphor and the LED both face one side of the LP filter. At high angles of incidence, the LP filter will not reflect the shortwave light. For this reason, the long wave bandedge of the LP filter can be placed at as long a wavelength as possible while blocking as little of the phosphor emission as possible. Again, the bandedge placement can be changed to optimize the overall system efficiency.

The term “adjacent” is defined herein to denote a relative positioning of two articles that are near one another. Adjacent items can be touching, or spaced away from each other with one or more materials disposed between the adjacent items.

LED excitation light can be any light that an LED source can emit. LED excitation light can be UV, or blue light. Blue light also includes violet and indigo light. LEDs include spontaneous emission devices as well as devices using stimulated or super radiant emission including laser diodes and vertical cavity surface emitting laser diodes.

Layers of phosphor described herein can be a continuous or discontinuous layer. The layers of phosphor material can be a uniform or non-uniform pattern. The layer of phosphor material can be plurality of regions having a small cross-sectional area such as, for example, a plurality of “dots” having an area in plan view of less than 10000 micrometers² or from 500 to 10000 micrometers². In an illustrative embodiment, the plurality of dots can each be formed from a phosphor which emits visible light at one or more different wavelengths such as, for example, a dot emitting red, a dot emitting blue, and a dot emitting green. The dots emitting visible light at a plurality of wavelengths can be arranged and configured in any uniform or non-uniform manner as desired. For example, the layer of phosphor material can be a plurality of dots with a non-uniform density gradient along a surface or an area. The “dots” can have any regular or irregular shape, and need not be round in plan view. Phosphor material can be in a co-extruded skin layer of the multilayer optical film.

Structured phosphor layers can be configured in several ways to provide benefits in performance, as described below. When multiple phosphor types are used to provide broader or fuller spectral output, light from shorter wavelength phosphors can be re-absorbed by other phosphors. Patterns comprising isolated dots, lines, or
5 isolated regions of each phosphor type reduce the amount of re-absorption. This would be particularly effective in cavity type constructions where unabsorbed pump light is reflected back to the phosphor pattern.

Multilayer phosphor structures can also reduce absorption. For example, it could be advantageous to form layers of each phosphor in sequence, with the longest
10 wavelength emitter nearest the excitation source. Light emitted nearer the emitter will on average, undergo multiple scattering within the total phosphor layer to a greater extent than light emitted near the output surface. Since the shortest wavelength emitted is most prone to scattering, it is advantageous to locate the shortest wavelength phosphor nearest to the output surface. In addition, it may be advantageous to use
15 different thicknesses for each layer, so as to compensate for the progressively lower intensity of the excitation light as it propagates through the multilayer structure. It would also be advantageous to place short pass filters in-between the different phosphor layers so as to reduce emitted phosphor light from scattering backward and being re-absorbed by phosphor layers earlier in the sequence.

20 Forming film structures with a phosphor coating also enables manufacturing of arrays of small structures suitable for dicing into individual units for diodes. For example, an array of small domes or hemispheres could be printed, each of which would be useful for reducing the "halo effect" sometimes present for PLED's (as described below).

25 Non-scattering phosphor layers can provide enhanced light output in combination with multilayer optical films. Non-scattering phosphor layers can comprise conventional phosphors in a substantially index-matched binder, or approximately index-matched binder (for example, a binder with high index inert nanoparticles), nanosize particles of conventional phosphor compositions (for

examples, where particle sizes are small and negligibly scatter light), or through the use of quantum dot phosphors. Quantum dot phosphors are light emitters based on semiconductors such as cadmium sulfide, wherein the particles are sufficiently small so that the electronic structure is influenced and controlled by the particle size. Hence, the absorption and emission spectra are controlled via the particle size. Quantum dots are disclosed in U.S. Patent No. 6,501,091, incorporated by reference herein.

Embodiments are disclosed herein where a first optical component comprising a phosphor/reflector assembly can be later attached to an LED base; a heat sink can optionally include a transparent heat sink to which the phosphor layer and interference filter may be attached. The transparent heat sink can be a layer of sapphire disposed between the phosphor layer/interference filter and the LED base. Most glasses have a higher thermal conductivity than polymers and can be useful in this function as well. Thermal conductivities of many other crystalline materials are higher than that of most glasses and can be used here also. The sapphire layer can be contacted at the edges by a metal heat sink.

In an illustrative embodiment, prior to coating the interference filter (i.e., polymeric interference filter with a phosphor layer) the surface of the filter can be treated to promote adhesion of the coating. The optimum treatment depends both on the surface layer of the filter and on the materials in the phosphor coating, specifically the binder used to hold the phosphor particles on the surface. The surface treatment can be a standard corona discharge treatment, or a corona discharge followed by a priming layer. The priming layer is typically less than 1 micron thick. Useful priming materials are PVDC, sulphonated polyesters and other amorphous polyesters such as Vitel, maleated copolymers such as Bynel (Dupont) and Admer (Mitsui Chemicals), and EVA such as Elvax (Dupont). Binders for the phosphor layer can be a thermoplastic and/or thermoformable and can be a fluoropolymer, or silicon based material, for example.

Alternative priming layers include, for example, vacuum coated layers, preferably from energetic sources such as ion-beam or gas plasma sources wherein the

ions or plasma components bombard the polymer surface while depositing the priming layer. Such priming layers are typically inorganic material layers such as titania or silica layers.

Although much attention has been given to the use of phosphors for down-
5 converting short wavelength light to visible light, it is also possible to up-convert infrared radiation to visible light. Up-converting phosphors are well known in the art and typically use two or more infrared photons to generate 1 visible photon. Infrared LEDs needed to pump such phosphors have also been demonstrated and are very efficient. Visible light sources that use this process can be made more efficient with
10 the addition of long-pass (LP) and short-pass (SP) filters although the functions of each are reversed in this case compared to the down-converting phosphor systems. A SP filter can be used to direct IR light towards the phosphor while transmitting the visible light, and an LP filter can be placed between the phosphor and LED to direct the emitted visible light outward towards the intended system or user.

15 The lifetime of an SP or LP filter or reflector is preferably greater than or equal to the lifetime of the LED in the same system. The degradation of a polymeric interference filter can be due to overheating which can cause material creep which changes the layer thickness values and therefore the wavelengths that the filter reflects. In the worst case, overheating can cause the polymer materials to melt, resulting in
20 rapid flow of material and change in wavelength selection as well as inducing non-uniformities in the filter.

Degradation of polymer materials can also be induced by short wavelength (actinic) radiation such as blue, violet or UV radiation, depending on the polymer material. The rate of degradation is dependent both on the actinic light flux and on the
25 temperature of the polymer. Both the temperature and the flux will in general, decrease with increasing distance from the LED. Thus it is advantageous in cases of high brightness LEDs, particularly UV LEDs, to place a polymeric filter as far from the LED as the design can allow. Placement of the polymer filter on a transparent heat sink as described above can also improve the lifetime of the filter. For domed filters,

the flux of actinic radiation decreases as the square of the distance from the LED. For example, a hemispherical MOF reflector with a 1 cm radius, placed with a unidirectional 1 watt LED at the center of curvature, would experience an average intensity of $1/(2\pi)$ Watts/cm² (surface area of the dome = 2π cm²). At a 0.5 cm radius, the average intensity on the dome would be four times of that value, or $2/\pi$ W/cm². The system of LED, phosphor, and multilayer optical film can be designed with light flux and temperature control taken into consideration.

A reflective polarizer can be disposed adjacent the multilayer reflector and/or adjacent the phosphor material. The reflective polarizer allows light of a preferred polarization to be emitted, while reflecting the other polarization. The phosphor layer and other film components known in the art can depolarize the polarized light reflected by the reflective polarizer, and either by the reflection from the phosphor layer, or phosphor layer in combination with the multilayer reflector, light can be recycled and increase the polarized light brightness of the solid state light device (LED). Suitable reflective polarizers include, for example, cholesteric reflective polarizers, cholesteric reflective polarizers with a $\frac{1}{4}$ wave retarder, DBEF reflective polarizer available from 3M Company or DRPF reflective polarizer also available from 3M Company. The reflective polarizer preferably polarizes light over a substantial range of wavelengths and angles emitted by the phosphor, and in the case where the LED emits blue light, may reflect the LED emission wavelength range as well.

Suitable multilayer reflector films are birefringent multilayer optical films in which the refractive indices in the thickness direction of two adjacent layers are substantially matched and have a Brewster angle (the angle at which reflectance of p-polarized light goes to zero) which is very large or is nonexistent. This allows for the construction of multilayer mirrors and polarizers whose reflectivity for p-polarized light decreases slowly with angle of incidence, are independent of angle of incidence, or increase with angle of incidence away from the normal. As a result, multilayer films having high reflectivity (for both planes of polarization for any incident direction in the case of mirrors, and for the selected direction in the case of polarizers) over a

wide bandwidth, can be achieved. These polymeric multilayer reflectors include alternating layers of a first and second thermoplastic polymer. The alternating layers defining a local coordinate system with mutually orthogonal x- and y-axes extending parallel to the layers and with a z-axis orthogonal to the x- and y-axes, and wherein at least some of the layers are birefringent. The absolute value of the difference in indices of refraction between the first and second layers is Δx , Δy , and Δz respectively, for light polarized along first, second, and third mutually orthogonal axes. The third axis is orthogonal to the plane of the film where Δx is greater than about 0.05, and where Δz is less than about 0.05. These films are described, for example, in U.S. Patent No. 5,882,774, which is incorporated by reference herein.

Non-planar is defined as a surface that is not flat. A non-planar surface can be formed, for example, by deflecting a flat article forming a curved article. The reflectors useful for the present invention can be planar or non-planar. The non-planar multilayer reflectors can be cast directly into a non-planar shaped article or thermoformed from a planar multilayer reflector into a non-planar multilayer reflector. The non-planar multilayer reflectors can be a concave shape. In an illustrative embodiment, the non-planar multilayer reflector can be a hemispherical concave shape. The LED can be located at or near the center of curvature of the non-planar multilayer reflector. In an illustrative embodiment, the non-planar multilayer reflector is a hemispherical concave shape opening towards the LED. The lateral extent of the light emitting region of the LED can be less than 1/3, or less than 1/6 of the minimum radius of curvature of the non-planar multilayer reflector.

FIG. 13 is a schematic sectional view of another embodiment of a PLED construction 210. A layer of phosphor material 222 is positioned to receive phosphor excitation light emitted by an LED 212. The LED 212 is described above and can emit excitation light at an excitation light wavelength. A TIR promoting layer 225 can be in contact with the layer of phosphor material 222. An interference reflector 224 can be positioned adjacent to the layer of phosphor material 222. FIG. 13 shows an interference reflector 224 positioned above the layer of phosphor material 222,

however the interference reflector 224 can be positioned below the layer of phosphor material 222, or above and below the layer of phosphor material 222. For example, a long pass interference reflector 224 can be positioned above the layer of phosphor material 222. The interference reflector 224 shown can reflect excitation light and transmit visible light emitted by the excited layer of phosphor material 222, as described above. The interference reflector 224 can reflect visible light emitted by the excited layer of phosphor material 222 and transmit excitation light emitted by the LED 212, as described above. The above arrangement can be disposed within an optically transparent body 220.

The layer of phosphor material 222 has a first index of refraction at the excitation light wavelength. In some embodiments, phosphor is dispersed within a binder and the binder has the first index of refraction. In other embodiments, phosphor is homogeneously distributed throughout the layer and the phosphor has the first index of refraction. This first index of refraction can be for example, 1.5 or greater, 1.5 to 1.9, or 1.5 to 1.7. The layer of phosphor material 222 can include a highly optically dispersive binder. Optically dispersive material includes for example, polyethylene terephthalate (PET), polycarbonate, or the like. The layer of phosphor material 222 can include an inorganic filler. The inorganic filler can be nano-particles of inorganic material that have a high dispersion index such as, for example, zirconium oxide, or titanium oxide. The inorganic filler can be sized from 1 to 1000 nm, or 10 to 100 nm. Alternatively or in addition, the optically dispersive binder can include nano-particles that are also optically active in down-converting the excitation light, such as "quantum dot" nano-clusters or semiconducting materials, for example, zinc sulphide, CdSe, or silicon nano-clusters.

A TIR promoting layer 225 can be in contact with the layer of phosphor material 222. Alternatively or in addition, the TIR promoting layer 225 can be positioned between the optically transparent body 220 and the layer of phosphor material 222. The TIR promoting layer 225 can be the same element as the optically transparent body 220 forming the encapsulant around the layer of phosphor material

222. The TIR promoting layer 225 can be positioned adjacent to the layer of phosphor material 222. The TIR promoting layer 225 has a second index of refraction that is less than the first index of refraction described above. This second index of refraction can be for example, less than 1.5, 1 to 1.5, or 1.2 to 1.4. The TIR promoting layer 225 can be any low index material such as, for example, air or gas, acrylates, olefins, silicones, or fluoropolymers. The optimum refractive index can be determined by experimentation, or estimated through optical modeling. Alternatively or in addition, this TIR promoting layer 225 may be placed on top and/or sides of the layer of phosphor material 222. The purpose of the TIR promoting layer 225 on the top of the layer of phosphor material 222 is to reduce the range of angles of light emitted by the phosphor, so as to improve collection efficiency of the lens, or to reduce the angles of light incidence on an interference reflector 224 placed above the layer of phosphor material 222. This TIR promoting layer 225 increases the efficiency and quality of light emitted by an LED package.

15 The optically transparent body 220 can have an index of refraction that is matched or substantially matched to the index of refraction of the layer of phosphor material 222 at the light wavelength emitted by the phosphor material. Alternatively or in addition, the layer of phosphor material 222 can have a substantially different index of refraction than the optically transparent body 220 and/or the TIR promoting layer 225 at the excitation light wavelength and substantially the same index of refraction at the visible light wavelength emitted by the excited phosphor. If the LED 212 emits light through a limited range of angles, e.g., by having less than a hemispherical emission, then the light from the LED 212 can be made to strike the layer of phosphor material 222/TIR promoting layer 225 interface at angles much less than 90 degrees. Preferably, the angle of incidence is less than the critical angle for total internal reflection (TIR) at the layer of phosphor material 222/TIR promoting layer 225 interface. The LED 212 emissions, once propagating in the layer of phosphor material 222, will undergo many scattering events, leading to a large range of propagating angles within that layer, including angles greater than the TIR angle. In

this manner, more of the short wavelength light can be confined to the layer of phosphor material 222 where it is eventually converted to longer wavelength light. Directional control of the light from the LED 212 can be achieved by a variety of techniques such as, for example, use of a microstructure on or within the LED 212 chip, or placement of the LED 212 in a reflective well that is designed to partially collimate the LED 212 emission.

By selecting an optically transparent body 220 with an index of refraction at the excitation wavelength less than that of the layer of phosphor material 222, the layer of phosphor material 222 will tend to trap a portion of the short wavelength or excitation light through TIR, and having TIR over a smaller range of angles for the long wavelength or visible light emitted by the phosphor. In an illustrative example, the layer of phosphor material 222 includes PET having an index of refraction of 1.73 at 380 nm and 1.665 at 580 nm. If this PET including layer of phosphor 222 is encapsulated in a resin having an index of 1.665, there will be no TIR for 580 nm light, and a 74° TIR angle for 380 nm light. Thus, this arrangement can increase the output efficiency of a phosphor converted LED.

The layer of phosphor material 222 and the interference reflector 224 can be planar, or non-planar. The layer of phosphor material 222 and the interference reflector 224 can be a concave and/or hemispherical shape facing the LED 212.

FIG. 14 is a schematic sectional view of another embodiment of a PLED construction 310. A layer of phosphor material 322 is positioned to receive phosphor excitation light emitted by an LED 312. The LED 312 is described above and can emit excitation light at an excitation light wavelength. A TIR promoting layer 325 can be positioned between the LED 312 and the layer of phosphor material 322. The TIR promoting layer 325 is described above. An interference reflector 326, as described above can be positioned adjacent to the TIR promoting layer 325. FIG. 14 shows an interference reflector 326 positioned between the LED 312 and the TIR promoting layer 325, however the interference reflector 326 can be positioned above the TIR promoting layer 325, or above and/or below the layer of phosphor material 322. For

example, a short pass interference reflector 326 can be positioned below the layer of phosphor material 322. The interference reflector 326 shown can reflect visible light emitted by the excited layer of phosphor material 322 and transmit excitation light, as described above. The above arrangement can be disposed within an optically transparent body 320, described above.

In another embodiment, similar results can be achieved even with an LED having a hemispherical emission pattern. In this case, the phosphor/TIR promoting layer interface is concave shaped and sized such that the LED emissive region is close to the center of curvature of the shaped interface. The geometry is illustrated in Figure 15.

FIG. 15 is a schematic sectional view of another embodiment of a PLED construction 410. A layer of phosphor material 422 is positioned to receive phosphor excitation light emitted by an LED 412. The layer of phosphor material 422 is shown as a concave and hemispherical shape facing the LED 412. The LED 412 is described above and can emit excitation light at an excitation light wavelength. A TIR promoting layer or first encapsulant 423 can be positioned between the LED 412 and the layer of phosphor material 422. The TIR promoting layer or first encapsulant 423, as described above, has an index of refraction at an excitation light wavelength that is less than the layer of phosphor material 422 index of refraction at an excitation light wavelength. In addition the TIR promoting layer or first encapsulant 423 can be an air gap. As described above.

An interference reflector (not shown), can be positioned adjacent to the layer of phosphor material 422, as described above. The above arrangement can be disposed within an optically transparent body 420. A first encapsulant 423 can be positioned between the phosphor layer 422 and LED 412. A second encapsulant 421 can be positioned adjacent the layer of phosphor material 422 on an opposing side of the layer of phosphor material 422. Thus, the optically transparent body

With this geometry, excitation light is incident on the layer of phosphor material 422 at angles close to zero degrees. After scattering within the layer of

phosphor material 422, the excitation light rays may strike the interface between the layer of phosphor material 422 and optically transparent body 420, or if present, the second encapsulant 421, at angles greater than the critical angle thereby confining the excitation light rays to the phosphor layer.

5 In addition to the use of dispersion to increase the degree of confinement of the primary wavelength light in the phosphor layer 422, further use of geometry and index differences can be utilized to improve the overall output of the secondary wavelength or visible light. Phosphors emit secondary wavelength light uniformly in all directions, which results in some light striking the phosphor 422/first encapsulant 423
10 interface at angles greater than the critical angle. This can be desirable on the back side of the phosphor layer if one desires that as much of the light as possible be emitted in a forward direction away from the LED 412. Referring to FIG. 15, it may be desirable to increase the index difference between the first encapsulant 423 and the phosphor layer 422 in order to reflect as much of the converted light as possible at that
15 interface. The use of an air gap between the first encapsulant 423 and the phosphor layer 422 will significantly decrease the critical angle for light propagating back toward the LED 412, resulting in TIR for more of the back-propagating light. With the proper geometry as discussed above, the incoming LED emissions will strike the same interface at lower average angles, with consequently lower reflectivity. The use of an
20 air gap or a low index for the first encapsulant 423 will therefore result in more light directed in the forward direction out of the LED/phosphor system.

 The low index layer also compliments the use of a multilayer optical short pass filter at the phosphor/first encapsulant 423 interface. At high angles of incidence, the MOF spectrum is shifted significantly to shorter wavelengths rendering it ineffective
25 for containing light emitted by the phosphor. Conversely, TIR effects work only at the higher angles of incidence. Therefore a combination of MOF and TIR can provide reflectance over a much greater range of angles than either of the two techniques can easily do alone.

On the front side of the phosphor layer 422, high transmission of the longer wavelength light is desirable. Thus, it is preferable that second encapsulant 421 have about the same index or greater index as the phosphor layer 422 for light with the secondary or visible wavelength. With the indices matched at the secondary
5 wavelength, all light emitted by the phosphor 422 can pass through that interface. Second encapsulant 421 can be shaped differently than the phosphor layer and the first encapsulant 423 to help circumvent TIR effects at the second encapsulant 421/air interface and thereby assist in extracting more light from the system.

FIG. 16 depicts a portion of still another PLED construction 510. This FIG.
10 shows a concept that can be applied beneficially to the other embodiments describes above. A micro-structured layer 528 can be positioned adjacent a layer of phosphor material 522. The micro-structured layer 528 can be positioned between the layer of phosphor material 522 and the LED 512. The micro-structured layer 528 has an index of refraction at an excitation light wavelength that is greater than a TIR promoting
15 layer 525 described below. The micro-structured layer 528 is shown having a prismatic microstructure.

A TIR promoting layer 525, as described above, is adjacent the micro-structured layer 528. The micro-structured interface formed between the TIR promoting layer 525 and the micro-structured layer 528 can reflect back visible light
20 rays emitted from the phosphor layer 522 at near normal angles and refracts rays at larger angles toward normal, except for rays propagating at angles greater than the values at which the rays strike the microstructure facets at normal incidence. At greater angles, the rays are refracted away from the normal. An optional additional TIR promoting layer 527 can be disposed between the layer of phosphor material 522
25 and the micro-structured layer 528 that will confine these higher angle rays within the phosphor layer, preventing their passage into the micro-structured layer and subsequent refraction away from the normal angle. A short pass reflector 526 can be positioned between the TIR promoting layer 525 and the LED 512. The short pass reflector 526 can reflect the refracted rays back toward the phosphor layer 522. The

above assembly is shown planar, however the above assembly can be non-planar or concave in shape.

Structural support to provide an air gap between the LED 512 and the phosphor layer 522, or between the LED encapsulant and the phosphor layer, can be provided for by edge support of the appropriate materials. If additional mechanical support is needed, a microstructured material such as one with e.g., ridges or posts, can be inserted between the appropriate layers, as described above. A feature of the support being an effective low index over the surface of one of the interfaces. Another example of a material having an extremely low effective index is an Aerogel. Aerogel is made by high temperature and pressure critical point drying of a gel composed of colloidal silica structural units filled with solvents. The resulting material is an underdense, microporous media. Air spaces in LED lighting systems could be filled with an Aerogel material to provide additional mechanical support. Such support may be useful in manufacturing for providing a spacer that creates an effective air gap in the manufacturing process even if the final product provides edge support of individual components.

EXAMPLES

Measurement of phosphor luminescence herein was made using a spectroradiometer (designated OL 770-LED by Optronic Laboratories, Inc., Orlando, Florida, USA) fitted with an integrating sphere (designated OL IS-670-LED by Optronic Laboratories) and a high precision LED holder (designated OL 700-80-20 by Optronic Laboratories). The spectroradiometer is calibrated to report the total radiant energy entering the integrating sphere at the input port (in units of Watts per nanometer). A 1 inch diameter disk was made from the phosphor coated sample using a custom punch. This disk fits into a custom film adaptor made to mount on the high precision LED holder. The custom adaptor holds the film sample approximately one inch above the base of the packaged LED. Measurements were performed by mounting an LED into the holder, placing the film with the phosphor coating into the adaptor, affixing the adaptor to the light-emitting diode mount and then inserting the diode mount assembly into the entrance aperture of the integrating sphere. If necessary, calibrated neutral density filters were used to adjust the light level reaching the detector of the spectroradiometer.

Unless otherwise stated, the multilayer optical films used in the following examples reflected both polarization states equally at normal incidence (i.e., each of the individual optical layers had nominally equal refractive indices along orthogonal in-plane axes).

For all of the following examples in which the thickness of the phosphor layer is given, the thickness was determined by subtracting the thickness of the substrate film from the thickness of the phosphor layer and substrate film together. The thicknesses were measured using a dial indicator (catalog number 52-520-140 by Fred V. Fowler Co., Inc., of Newton, Massachusetts, USA) with a flat contact point (catalog number 52-525-035, also from Fowler) mounted on a dial gage stand (catalog number 52-580-020, also from Fowler). The thickness of the substrate film was the average of three measurements at random locations on the substrate film. The thickness of the

phosphor layer and substrate film was the average of six measurements taken at random locations on the phosphor layer.

Example 1

5 A coating of cerium-doped yttrium aluminum garnet (YAG:Ce) phosphor was made on single layer clear poly(ethylene terephthalate) (PET) film by the following procedure.

12.00 grams of fluoropolymer resin (designated "Phosphor Ink Part A: Resin Solution", part number: 11NR001, rev: AA, batch number: KY4-035 by Durel
10 Company of Chandler, Arizona, USA) was placed into a 40 milliliter glass jar. 15.02 grams of YAG:Ce phosphor (designated QMK58/F-U1 Lot #13235 by Phosphor Technology, Ltd. of Stevenage, England) was measured into a weighing dish. The phosphor was mixed into the resin by first adding one-half of the phosphor to the resin and mixing it in by hand with a stainless steel spatula and then adding the other half
15 and mixing it by hand. The phosphor and resin were mixed by hand until the mixture had a smooth texture and uniform appearance. The jar containing the resulting phosphor paste was covered with a lid and placed on a bottle roller for about 30 minutes.

A sheet of single layer clear PET film 3M Company (St. Paul, MN) 6 inches
20 wide by 10 inches (250 micrometers) long by 1.5 mils (40 micrometers) thick was placed on a clean flat surface. Both surfaces of the PET film were wiped with a lint-free cotton cloth dampened with methanol. The jar containing the phosphor paste was removed from the bottle roller and about 5 grams of paste was placed into a small puddle on the PET film. The phosphor paste was hand-drawn into a coating using the
25 5 mil (130 micrometers) gap of a square multiple clearance applicator (designated PAR-5357 by BYK-Gardner USA of Columbia, Maryland, USA). The wet film was cured at a temperature of about 130 °C for 30 minutes in a gravity convection oven (designated Model 1350G by VWR International, Inc., of West Chester, Pennsylvania,

USA). After curing, the phosphor/resin coating thickness was 1.6 mils (40 micrometers).

5 A 1 inch (25 mm) diameter disk of the YAG:Ce coated film was prepared and mounted into the spectroradiometer as described above. The disk was oriented with the phosphor coated side facing into the integrating sphere. A blue LED (designated Part #25-365 by Hosfelt Electronics, Inc., Steubenville, OH) with a peak wavelength of about 463 nm was used to excite the phosphor. The standard 5 mm package for the blue LED was modified by machining off the domed lens at the top of the package to provide a flat exit face for the blue light. Approximately 0.18 inch (4.6 mm) of the package was removed from the top of the package. The LED was powered at 20 milliamps and 3.46 volts by a constant current power supply. The emission spectra of the phosphor layer recorded using the spectroradiometer is shown in Figure 16 as the curve labeled "Example 1". Using software supplied with the spectroradiometer, the total luminous flux emitted into the integrating sphere was calculated to be 0.068 lumens.

Example 2

20 A piece of multi-layer optical film (MOF) having alternating layers of PET and co-PMMA and having a normal-incidence reflection band (measured at half-maximum) from about 600 nm to about 1070 nm (made in accordance with U.S. Patent No. 6,531,230) was placed in the film adaptor between the phosphor coated PET film of Example 1 and the blue LED of Example 1 (operated at 20 milliamps). The spectrum was recorded and is shown in Figure 16 as the curve labeled "Example 2". Using software supplied with the spectroradiometer, the total luminous flux emitted into the integrating sphere was calculated to be 0.118 lumens. This represents an increase in luminous intensity of 73%.

Example 3

A coating of zinc sulfide (ZnS) phosphor was made on poly (ethylene terephthalate) (PET) film by the following procedure:

20.04 grams of fluoropolymer resin (designated "Phosphor Ink Part A: Resin Solution", part number: 1INR001, rev: AA, batch number: KY4-035 by Durel Company of Chandler, Arizona, USA) was placed into a 2 ounce glass jar. 20.06 grams of ZnS phosphor (designated GL29A/N-C1 Lot #11382 by Phosphor Technology, Ltd. of Stevenage, England) was measured into a weighing dish. The phosphor was mixed into the resin by first adding one-half of the phosphor to the resin and mixing it in by hand with a stainless steel spatula and then adding the other half and mixing it by hand. The phosphor and resin were mixed by hand until the mixture had a smooth texture and uniform appearance. The jar containing the resulting phosphor paste was covered with a lid and placed on a bottle roller for about 24 hours.

A sheet of clear PET film by 3M Company (St. Paul, MN) 6 inches wide by 10 inches long by 1.5 mils (45 micrometers) thick was placed on a clear flat surface. Both surfaces of the PET film were wiped with a lint-free cotton cloth dampened with methanol. The jar containing the phosphor paste was removed from the bottle roller and about 3 grams of paste was placed onto the PET film. The phosphor paste was hand-drawn into a coating using the 2 mil (50 micrometers) gap of a square multiple clearance applicator (designated PAR-5353 by BYK-Gardner USA of Columbia, Maryland, USA). The wet film was cured at a temperature of about 130 °C for 30 minutes in a gravity convection oven (designated Model 1350G by VWR International, Inc., of West Chester, Pennsylvania, USA). After curing the phosphor/resin coating thickness was 0.7 mils (18 micrometers).

A one inch (25 mm) diameter disk of the ZnS coated film was prepared and mounted into the spectroradiometer as described above. The disk was oriented with the phosphor coated side facing into the integrating sphere. A UV LED (designated Part #25-495 by Hosfelt Electronics, Inc of Steubenville, OH) with a peak wavelength of about 395 nm was used to excite the phosphor fluorescence. The standard 5 mm package for the UV LED was modified by machining off the domed top of the package

to provide a flat exit face for the UV light. Approximately 0.18 inches (5 mm) of the package was removed from the top of the package. The LED was powered at 20 milliamps and 3.7 volts by a constant current power supply. The emission spectra of the phosphor layer recorded using the spectroradiometer is shown in Figure 17 as the curve labeled "Example 3". Using software supplied with the spectroradiometer, the total luminous flux emitted into the integrating sphere was calculated to be 0.052 lumens.

Example 4

A piece of multi-layer optical film (MOF) having alternating layers of PET and co-PMMA and having a normal-incidence reflection band (measured at half-maximum) from about 320 nm to about 490 nm (made in accordance with U.S. Patent No. 6,531,230) was placed in the film adaptor on top of the phosphor layer of Example 3, and the UV LED of Example 3 (operated at 20 milliamps) was used as the excitation source. The spectrum was recorded and is shown in Figure 17 as the curve labeled "Example 4". Using software supplied with the spectroradiometer, the total luminous flux emitted into the integrating sphere was calculated to be 0.062 lumens. This represents an increase in luminous intensity when compared to Example 3 of about 19%.

Example 5

A broadband visible reflector was made by laminating two pieces of multi-layer optical film (MOF). A layer of MOF having alternating layers of PET and co-PMMA and a normal-incidence reflection band (measured at half-maximum) from about 490 nm to about 610 nm (manufactured by 3M Company of St. Paul, MN) was laminated to a layer of MOF having alternating layers of PET and co-PMMA and having a normal-incidence reflection band (measured at half-maximum) from about 590 nm to about 710 nm (manufactured by 3M Company of St. Paul, MN) using an optically clear adhesive. The laminate was placed in the film adaptor between the phosphor coated PET film of Example 3, and the UV LED of Example 3 (operated at

20 milliamps). A piece of multi-layer optical film (MOF) having alternating layers of PET and co-PMMA and having a normal-incidence reflection band (measured at half-maximum) from about 320 nm to about 490 nm (manufactured by 3M Company of St. Paul, MN) was placed in the film adaptor on top of the phosphor layer to create a cavity having a phosphor layer sandwiched between a visible mirror on the LED side and a UV/blue mirror on the other side. The spectrum was recorded and is shown in Figure 17 as the curve labeled "Example 5". Using software supplied with the spectroradiometer, the total luminous flux emitted into the integrating sphere was calculated to be 0.106 lumens. This represents an increase in luminous intensity when compared to Example 3 of about 104%.

Example 6

A coating of zinc sulfide (ZnS) phosphor was made on poly (ethylene terephthalate) (PET) film by the following procedure:

The phosphor paste described in Example 3 was coated onto a sheet of clear PET film 6 inches wide by 10 inches long by 1.5 mils (40 micrometers) thick. The PET was placed on top of a clean flat surface. Both surfaces of the PET film were wiped with a lint-free cotton cloth dampened with methanol. About 3 grams of paste was placed onto the PET film. The phosphor paste was hand-drawn into a coating using the 4 mil (100 micrometer) gap of a square multiple clearance applicator (designated PAR-5353 by BYK-Gardner USA of Columbia, Maryland, USA). The wet film was cured at a temperature of about 130 °C for 30 minutes in a gravity convection oven (designated Model 1350G by VWR International, Inc., of West Chester, Pennsylvania, USA). After curing, the phosphor/resin coating thickness was 1.3 mils (33 micrometers).

A one inch (25.4 mm) diameter disk of the ZnS coated film was prepared and mounted into the spectroradiometer as described above. The disk was oriented with the phosphor coated side facing into the integrating sphere. A UV LED (designated Part #25-495 by Hosfelt Electronics, Inc of Steubenville, OH) with a peak wavelength

of about 395 nm was used to excite the phosphor. The standard 5 mm package for the UV LED was modified by machining off the domed top of the package to provide a flat exit face for the UV light. Approximately 0.18 inches (5 mm) of the package was removed from the top of the package. The LED was powered at 20 milliamps and 3.7 volts by a constant current power supply. The emission spectra of the phosphor layer recorded using the spectroradiometer is shown in Figure 18 as the curve labeled “Example 6”. Using software supplied with the spectroradiometer, the total luminous flux emitted into the integrating sphere was calculated to be 0.066 lumens.

10 **Example 7**

A piece of multi-layer optical film (MOF) having alternating layers of PET and co-PMMA and having a normal-incidence reflection band (measured at half-maximum) from about 490 nm to about 610 nm (manufactured by 3M Company of St. Paul, MN) was placed in the film adaptor between the phosphor coated PET film of Example 6 and the UV LED of Example 6 (operated at 20 milliamps). The spectrum was recorded and is shown in Figure 18 as the curve labeled “Example 7”. Using software supplied with the spectroradiometer, the total luminous flux emitted into the integrating sphere was calculated to be 0.095 lumens. This represents an increase in luminous intensity when compared to Example 6 of about 44%.

20

Example 8

A coating of zinc sulfide (ZnS) phosphor was made on multi-layer optical film (MOF) by the following procedure:

The phosphor paste described in Example 3 was coated onto a sheet of MOF having alternating layers of PET and co-PMMA and having a normal-incidence reflection band (measured at half-maximum) from about 490 nm to about 610 nm (manufactured by 3M Company of St. Paul, MN). The MOF was placed on top of a clean flat surface. Both surfaces of the MOF film were wiped with a lint-free cotton cloth dampened with methanol. About 3 grams of paste was placed onto the MOF

film. The phosphor paste was hand-drawn into a coating using the 4 mil gap (100 micrometers) of a square multiple clearance applicator (designated PAR-5353 by BYK-Gardner USA of Columbia, Maryland, USA). The wet film was cured at a temperature of about 130 °C for 30 minutes in a gravity convection oven (designated
5 Model 1350G by VWR International, Inc., of West Chester, Pennsylvania, USA). After curing, the phosphor/resin coating thickness was 1.3 mils (33 micrometers).

A one inch diameter disk of the ZnS coated film was prepared and mounted into the spectroradiometer as described above. The disk was oriented with the phosphor coated side facing into the integrating sphere. A UV LED (designated Part
10 #25-495 by Hosfelt Electronics, Inc of Steubenville, OH) with a peak wavelength of about 395 nm was used to excite the phosphor. The standard 5 mm package for the UV LED was modified by machining off the domed top of the package to provide a flat exit face for the UV light. Approximately 0.180 inches (5 mm) of the package was removed from the top of the package. The LED was powered at 20 milliamps and 3.7
15 volts by a constant current power supply. The emission spectra of the phosphor layer recorded using the spectroradiometer is shown in Figure 18 as the curve labeled “Example 8”. Using software supplied with the spectroradiometer, the total luminous flux emitted into the integrating sphere was calculated to be 0.107 lumens. This represents an increase in luminous intensity when compared to Example 6 of about
20 62%.

Example 9

A coating of zinc sulfide (ZnS) phosphor was screen printed on the laminated multi-layer optical film (MOF) described in Example 5 by the following procedure:
25 150 grams of fluoropolymer resin (designated “Phosphor Ink Part A: Resin Solution”, part number: 11NR001, rev: AA, batch number: KY4-035 by Durel Company of Chandler, Arizona, USA) was placed into a 16 ounce glass jar. 150 grams of ZnS phosphor (designated GL29A/N-C1 Lot #11382 by Phosphor Technology, Ltd. of Stevenage, England) was measured into a weighing dish. The

phosphor was slowly mixed into the resin using a glass impeller driven by an air motor. The phosphor and resin were mixed until the mixture had a smooth texture and uniform appearance. The jar containing the resulting phosphor paste was covered with a lid and placed on a bottle roller for about 10 minutes.

5 The printing was done using a halftone pattern with a resolution of 28 lines per inch (1.1 lines per mm) on a 280 thread per inch (11 thread per mm) PET screen mounted on a screen printer (designated Type SSM by Svecia Silkscreen Maskiner AB, of Stockholm, Sweden). The halftone pattern consisted of three regions having 10%, 50% and 90% coverage. The pattern was printed in one pass onto a sheet of the
10 two laminated MOF films described in Example 5.

 The printed layer was cured at a temperature of about 138 °C for 15 minutes in a forced air oven. After curing, the phosphor/resin coating thickness was 0.8 mils (20 micrometers).

 A one inch (25 mm) diameter disk of the ZnS screen printed film from the
15 portion of the pattern having 50% coverage was prepared and mounted into the spectroradiometer as described above. The disk was oriented with the phosphor coated side facing into the integrating sphere. A UV LED (designated Part #25-495 by Hosfelt Electronics, Inc of Steubenville, OH) with a peak wavelength of about 395 nm was used to excite the phosphor. The standard 5mm package for the UV LED was
20 modified by machining off the domed top of the package to provide a flat exit face for the UV light. Approximately 0.180 inches (5 mm) of the package was removed from the top of the package. The LED was powered at 20 milliamps and 3.7 volts by a constant current power supply. The emission spectra of the phosphor layer recorded using the spectroradiometer is shown in Figure 19 as the curve labeled "Example 9".
25 Using software supplied with the spectroradiometer, the total luminous flux emitted into the integrating sphere was calculated to be 0.052 lumens.

Example 10

A piece of multi-layer optical film (MOF) having alternating layers of PET and co-PMMA and having a normal-incidence reflection band (measured at half-maximum) from about 320 nm to about 490 nm (manufactured by 3M Company of St. Paul, MN) was placed in the film adaptor on top of the phosphor layer of Example 9, and the UV LED of Example 9 (operated at 20 milliamps) was used as the excitation source. The spectrum was recorded and is shown in Figure 19 as the curve labeled "Example 10". Using software supplied with the spectroradiometer, the total luminous flux emitted into the integrating sphere was calculated to be 0.078 lumens. This represents an increase in luminous intensity when compared to Example 9 of about 50%.

Example 11

A thermoformed dome of multilayer optical film (MOF) coated with zinc sulfide (ZnS) phosphor was made by the following procedure.

A layer of MOF having alternating layers of PET and co-PMMA and having a normal-incidence reflection band (measured at half-maximum) from about 590 nm to about 710 nm (manufactured by 3M Company of St. Paul, Minnesota, USA) was bonded to a sheet of poly (vinyl chloride) to form a flexible composite. This composite will be referred to as MOF-PVC.

The MOF-PVC was placed on a clean flat surface with the MOF side facing up. The top surface of the MOF-PVC was wiped with a lint free cotton cloth dampened with methanol. About 3 grams of the ZnS phosphor paste described in Example 9 was placed onto the MOF-PVC. The phosphor paste was hand-drawn into a coating using the 4 mil (100 micrometer) gap of a square multiple clearance applicator (designated PAR-5353 by BYK-Gardner USA of Columbia, Maryland, USA). The wet film was cured at a temperature of about 130 °C for 30 minutes in a gravity convection oven (designated Model 1350G by VWR International, Inc., of West Chester, Pennsylvania, USA).

The phosphor coated MOF-PVC composite was loaded into a thermoforming machine. The layer was heated for 23 seconds at a temperature of 270 °C. Using a plate with a circular aperture (about ½ inch (13 mm) diameter) the phosphor coated MOF-PVC was formed into a hemisphere of about 1/2 inch (13 mm) with the phosphor on the convex side of the hemisphere. Visual inspection of the hemisphere indicated the hemisphere had a greater thickness near an outer region of the hemisphere and was thinner at an inner region of the hemisphere. The phosphor layer was smooth and continuous and exhibited no signs of cracking or delamination.

10 **Example 12**

A thermoformed dome of multilayer optical film (MOF) coated with zinc sulfide (ZnS) phosphor was made by the following procedure.

A sheet of MOF-PVC described in Example 11 was placed on a clean flat surface with the MOF side facing up. The top surface of the MOF-PVC was wiped with a lint free cotton cloth dampened with methanol. About 3 grams of the ZnS phosphor paste described in Example 9 was placed onto the MOF-PVC. The phosphor paste was hand-drawn into a coating using the 2 mil (50 micrometer) gap of a square multiple clearance applicator (designated PAR-5353 by BYK-Gardner USA of Columbia, Maryland, USA). The wet film was cured at a temperature of about 130 °C for 30 minutes in a gravity convection oven (designated Model 1350G by VWR International, Inc., of West Chester, Pennsylvania, USA).

The phosphor coated MOF-PVC composite was loaded into a thermoforming machine. The layer was heated for 21 seconds at a temperature of 270 °C. Using a plate with a circular aperture (about ½ inch (13 mm) diameter) the phosphor coated MOF-PVC was formed into a hemisphere of about 1/2 inch (13 mm) with the phosphor on the convex side of the hemisphere. Visual inspection of the hemisphere indicated the hemisphere had a greater thickness near an outer region of the hemisphere and was thinner at an inner region of the hemisphere. The phosphor layer was smooth and continuous and exhibited no signs of cracking or delamination.

Example 13

A thermoformed dome of multilayer optical film (MOF) coated with cerium-doped yttrium aluminum garnet (YAG:Ce) phosphor was made by the following procedure.

20.01 grams of fluoropolymer resin (designated "Phosphor Ink Part A: Resin Solution", part number: 1INR001, rev: AA, batch number: KY4-035 by Durel Corporation of Chandler, Arizona, USA) was placed into a 2 ounce glass jar. 19.98 grams of YAG:Ce phosphor (designated QMK58/F-U1 Lot #13235 by Phosphor Technology, Ltd. of Stevenage, England) was measured into a weighing dish. The phosphor was mixed into the resin by first adding one-half of the phosphor to the resin and mixing it in by hand with a stainless steel spatula and then adding the other half and mixing it by hand. The phosphor and resin were mixed by hand until the mixture had a smooth texture and uniform appearance. The jar containing the resulting phosphor paste was covered with a lid and placed on a bottle roller for about 30 minutes.

A sheet of MOF-PVC described in Example 11 was placed on a clean flat surface with the MOF side facing up. The top surface of the MOF-PVC was wiped with a lint free cotton cloth dampened with methanol. About 3 grams of the YAG:Ce phosphor paste was placed onto the MOF-PVC. The phosphor paste was hand-drawn into a coating using the 4 mil (100 micrometer) gap of a square multiple clearance applicator (designated PAR-5353 by BYK-Gardner USA of Columbia, Maryland, USA). The wet film was cured at a temperature of about 130 °C for 30 minutes in a gravity convection oven (designated Model 1350G by VWR International, Inc., of West Chester, Pennsylvania, USA).

The phosphor coated MOF-PVC composite was loaded into a thermoforming machine. The layer was heated for 23 seconds at a temperature of 270 °C. Using a plate with a circular aperture (about ½ inch (13 mm) diameter) the phosphor coated MOF-PVC was formed into a hemisphere of about 1/2 inch (13 mm) with the

phosphor on the convex side of the hemisphere. Visual inspection of the hemisphere indicated the hemisphere had a greater thickness near an outer region of the hemisphere and was thinner at an inner region of the hemisphere. The phosphor layer was smooth and continuous and exhibited no signs of cracking or delamination.

5

Example 14

A thermoformed dome of multilayer optical film (MOF) coated with cerium-doped yttrium aluminum garnet (YAG:Ce) phosphor was made by the following procedure.

10 A sheet of MOF-PVC described in Example 11 was placed on a clean flat surface with the MOF side facing up. The top surface of the MOF-PVC was wiped with a lint free cotton cloth dampened with methanol. About 3 grams of the YAG:Ce phosphor paste described in Example 13 was placed onto the MOF-PVC. The phosphor paste was hand-drawn into a coating using the 2 mil (50 micrometer) gap of
15 a square multiple clearance applicator (designated PAR-5353 by BYK-Gardner USA of Columbia, Maryland, USA). The wet film was cured at a temperature of about 130 °C for 30 minutes in a gravity convection oven (designated Model 1350G by VWR International, Inc., of West Chester, Pennsylvania, USA).

The phosphor coated MOF-PVC composite was loaded into a thermoforming
20 machine. The layer was heated for 21 seconds at a temperature of 270 °C. Using a plate with a circular aperture (about ½ inch (13 mm) diameter) the phosphor coated MOF-PVC was formed into a hemisphere of about 1/2 inch (13 mm) with the phosphor on the convex side of the hemisphere. Visual inspection of the hemisphere indicated the hemisphere had a greater thickness near an outer region of the
25 hemisphere and was thinner at an inner region of the hemisphere. The phosphor layer was smooth and continuous and exhibited no signs of cracking or delamination.

Example 15

A sheet of MOF-PVC described in Example 11 was heated in the thermoforming device described above to a temperature of about 270 °C for 16 seconds. This heated sheet of MOF-PVC was draped over the hemispherical lens of a commercially available 5 mm LED package with vacuum assist. The MOF-PVC
5 acquired a final shape corresponding to the hemispherical lens shape.

The formed MOF-PVC transmission spectrum was measured using a Perkin-Elmer Lambda 19 spectrophotometer. The spectrum of the central portion of the formed MOF-PVC was shown to have band edges at 360 nm and 460 nm with a peak reflectivity occurring at 400 nm. This formed MOF-PVF had a transmission greater
10 than 75% at wavelengths above 500 nm. This measured spectral shift of the MOF-PVC was due to the thinning of the optical stack occurring during the shaping operation.

All patents and patent applications referenced herein are incorporated by
15 reference in their entirety. Various modifications and alterations of this invention will be apparent to those skilled in the art without departing from the scope and spirit of this invention, and it should be understood that this invention is not limited to the illustrative embodiments set forth herein.